

PAVLOV, N., inzh. (Minsk); ARKUSH, N., inzh. (Riga); MIKN, E., mekhanik
(Tallin); MYAGI, N. [Magi, N.], mekhanik (Tallin); LIBERMAN,
V. (Lyubertsy Moskovskoy obl.); ZHURAVLEV, G., tekhnolog

Proposed, made, introduced. Izobr. i rats. no.8:12-13 Ag
'62. (MIRA 15:9)

(Technological innovations)

ROZHDELYVENSKIY, V.: PIVION, N., master sports; NHRAERYKH, Sverlans, sportsmenks I razryada

A student amateur club. Kryl.rod. 1º no.c.9-10 Je to.

(M.Fa 19a1)

1. Fredsedstel* planernoy sektsis studencheskogo samodeyatel*.
nogo kluba highvahevskogo avietsi omogo instituta (for Rozhdestvenskiy). 2. Hukovoqitel* eviamodel*noy laboratoris studencheskogo samodeyatel*nogo kluba Kuyhyehevskogo avistsionnogo instituta (for Favlov).

PAVLOV, Meg. insh.

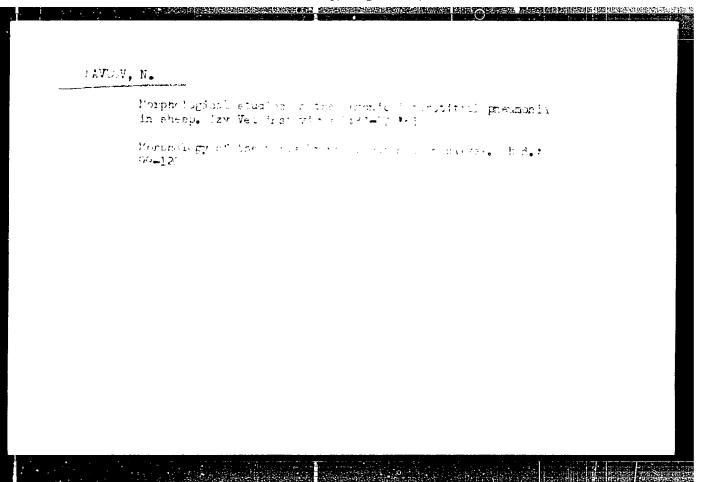
Achievements of the East-German motorcycle industry. Za rul. 20 no.5:16-17 My 162. (MIRA 16:4)

(Germany, East-Motorcycle industry)

PAVLOV, N., polkovník v otstavke

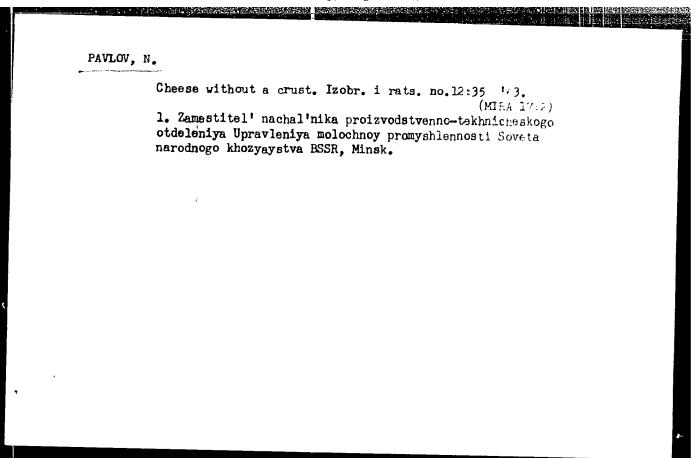
Russian artillery in the battle of Borodimo. Voen.vest. 42
no.9:25-26 S *62. (MIRA 15:8)

(Borodino, Battle of, 1812)



PAVLOV, N.; PETROVA, A.

Morphological changes in the experimental intoxication of rats with methyl alcohol and nicotine (separately or combined). Izv Vet inst virus 2:121-134 *63



一年了多年的 经营工工程 经营工程 医

BABIY, Ye.; ZYUBIN, S.; ANTYUKHOV, A.; KAMCHATOV, K.; DOLGOVA, L.; KASTOR-NOV, M., mekhanik; GOL'TSEV, M.; KUZ'MIN, I., mekhanik; PAVLOV, N., mashinist kombayna; SMETANKIN, P., mashinist kombayna; SAFONOV, M., mashinist kombayna; KOZLOV, N., brigadir gornorabochikh; BUYAK, I., brigadir gornorabochikh; SOLDATOV, N., brigadir gornorabochikh

Not into the records but into practice. Sov.shakht. 12 no.12:1718 D '63. (MIRA 17:3)

1. Shakhtoupravleniye No.3-25 tresta Donskoyugol' kombinata Tulaugol'. 2. Nachal'nik shakhtoupravleniya No.3-25 tresta Donskoyugol'
kombinata Tulaugol' (for Babiy). 3. Sekretar'partorganizatsii shakhtoupravleniya No.3-25 tresta Donskoyugol' kombinata Tulaugol' (for
Zyubin). 4. Glavnyy inzh. shakhtoupravleniya No.3-25 tresta Donskoyugol' kombinata Tulaugol' (for Kamchatov). 5. Sekretar' komsomol'skoy organizatsii shakhtoupravleniya No.3-25 tresta Donskoyugol'
kombinata Tulaugol' (for Dolgova).

Veterinary Medicine

BULGARIA

PAVLOV, N., Dr., MAKAVEYEVA, E., Dr., VESELINOVA, A., Dr., VIZPB/not

"Disease of New- Born lambs Caused By Neorickettsiae"

Sofia, Veterinarna Sbirka, Vol 63, No 1, 1966, pp 3-6 Abstract: The virus abortion of sheep is a latent neorickettsiae infection. Jambs that are born alive exhibit symptoms of the infection. Tissues and organs of infected new-born lambs were subjected to a pathological, anatomic, and histologic investigation. Two strains of the causative factor were isolated and propagated in 6-day old chicken embryos on being injected into their yolk sac. The embryos perished on infection and showed presence of typical elementary bodies. Antigen obtained from chicken embryos had properties identical with those of antigen isolated from the placenta of aborting ewes. By using the antigen from chicken embryos, the reaction of complement fixation was carried out for diagnostic purposes.

AP**PROWED** FOR RELEASE: Tuesday, August 01, 2000 CIA-RDP86-00513R001239

Reliance on active membership. Radio no.10:7 0 '53.

(MIRA 6:10)

1. Leningradskiy gorodskoy radioklub Vsesoyuznogo dobrovol'nogo obshchestva sodeystviya armii, aviatsii i flotu. (Radio clubs)

PAVIOV. N., red. [Views of Smolensk; an album] Vidy Smolenska . Al'bum, Smolensk, Smolenskoe knizhnoe izd-vo, 1959. 2 p., 30 plates.

(MIRA 15:4) (Smolensk--Views)

"APPROVED FOR RELEASE: Tuesday, August 01, 2000

CIA-RDP86-00513R001239

L 04484_67 FSS-2/EWT(1) TT/GW ACC NR: AN6010454 (N) SOURCE CODE: UR/9008/66/000/080/0008/0008

AUTHOR: Ivanov, Ye. (Engineer); Pavlov, N. (Engineer)

ORG: none

TITLE: Lunar artificial satellite

SOURCE: Krasnaya zvezda, no. 80, 06 Apr 66, p. 8, col. 1-7

TOPIC TAGS: lunar flight, lunar mission, lunar satellite, artificial satellite, SATELLITE TRAJECTORY, GRAVITATION EFFECT

ABSTRACT: The authors comment on the reconnaissance mission of the Luna-16 artificial satellite launched on 3 April 1966 and discuss the computation problems connected with the flight. Figures concerning launch, trajectory, and orbital velocity, and altitude are presented in the original article. The number of revolutions and altitude needed for a complete reconnaissance of the moon's surface are given with various alternatives, and are compared with those valid for the earth artificial satellites. The first and second flight stages deal with overcoming gravitation and setting the spacecraft in a trajectory toward the moon, while the third stage of the flight in which the retroacting power plant was actuated to slow down the vehicle and

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1. 04486-57

ACC NR: AN6010454

set it into a computed lunar orbit is discussed in more detail, including the timing and power requirement for correcting deviations from the earth-moon section of the flight trajectory. Factors such as the gravity influence of the sun and other planets upon the satellite trajectory and the absence of lunar atmosphere are discussed. The upon the satellite trajectory and the absence of lunar satellites which, in addition authors also speculate about future use of artificial lunar satellites which, in addition to gathering information on the lunar mass, shape, surface, and surrounding space, are likely to include radio-relaying in long-distance communication systems includarelikely to include radio-relaying in long-distance communication systems including TV, replace, to a certain extent, the function of the earth's ionosphere and serve as orbital stations supplying moon explorers with necessary logistics. [KP]

SUB CODE: 22/ SUBM DATE: none/

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AUTHORS:

Fogel A.A Pavlov N.A Korkin I V and Sidorova

T.A. (Leningrad)

TITLE

Inductors for heating and melting metals in the

levitated condition

PERIODICAL: Akademiya nauk SSSR, Izvestiya Otdeleniye tekhnicheskikh

nauk. Metallurgiya i toplivo, no.5, 1961, 51-61

TEXT: The practice of heating levitated metals suspended freely in an electromagnetic field is increasing, but many practical problems remain unsolved. This article considers the influence of the frequency and configuration of the electromagnetic field on the heating of a metallic body suspended in it. Expressions are written for the relationship between the electromagnetic pressure on the levitated metal and the specific power transmitted to it. The formulae show that by altering the frequency and intensity of the magnetic field the electromagnetic pressure on the metal may be changed without altering the power transmitted to it. In the case of a freely-suspended metallic body the force applied by the field is equal to the weight of the body

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Thus, by altering the frequency it is possible to regulate the power transmitted to the metal and so its temperature. The effect is not strictly a surface one, as the metal has some 'transparency' to the field. Elementary consideration is therefore given to the case of induction heating of a metal plate in a longitudinal plane parallel magnetic field. Formulae are derived for the power transmitted per unit surface of plate, for the electromagnetic pressure on the plate and for the ratio of pressure to power. These expressions are used to construct the curves shown in Fig.1 in which the power transmitted to the plate (curve 1), the electric field strength (curve 2) and the magnetic field strength (curve 3) are plotted as functions of field frequency with a constant electromagnetic pressure on the plate surface (F = const) The depth of penetration and constant plate thicknes (d = const) For a levitated of the electromagnetic energy $\triangle = \sqrt{PP}/\pi \mu f$ body the necessary electromagnetic force is determined by its weight. The power required for heating depends mainly on the temperature required because as there is no thermal insulation. thermal equilibrium is established very quickly, within two or three minutes. The graph of Fig.l shows that for a given body

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with constant electromagnetic pressure applied to it the power increases with the frequency, so that to raise the temperature the frequency should be raised. The limiting frequency depends on the maximum permissible electrical field intensity at the body surface or on the associated voltage on the inductor. The maximum permissible electrical field intensity should be less than that which causes electrical breakdown and this depends on the properties of the gaseous medium surrounding the inductor. If, with constant electromagnetic pressure, the frequency is reduced then the magnetic field strength must be increased, that is to say, the inductor current must be increased. The limit in this case depends on the permissible current density in the inductor conductors. Thus for a metal body of given size there is a definite range of frequency within which the body can be suspended in the electromagnetic field The choice of frequency depends on the temperature required and by altering the frequency within this range it is possible to control the limiting temperature of the metal whilst maintaining it in the levitated condition. When a fixed metal body is heated by induction there is a direct

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relationship between the power applied to the inductor and that transmitted to the body. But in the case of a body of levitated metal an allowance must be made for the configuration of the field set up by the inductor, because the configuration determines the nature of the relationship between the power applied to the inductor and that transmitted to the metal The power transmitted to the metal body is related to the pressure applied to it by the magnetic field. Both the power and the electromagnetic pressure depend upon the magnetic field intensity at the body surface. If the body is levitated, the vertical component equals the weight of the body and the horizontal is zero. Evidently to support the weight of a freely suspended metal body the field intensity under the body should be greater than that above it In a more uniform field a higher overall field intensity is necessary to support the body. Thus a greater power is transmitted to the body in the more uniform field. If the power applied to the inductor is altered, the position of the body may alter If it moves vertically but without any change in the field at its surface there will be no change in the power transmitted to the body. Card 4/12

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if in moving vertically it passes from a field of one configuration to that of another, then as the power applied to the inductor is increased, that transmitted to the body may increase or decrease, depending upon the configuration of the field. A brief analysis is then made of the field between the two conductors with current flowing in opposite directions. The force acts perpendicular to the direction of the magnetic field so it is the horizontal component of the field that governs the vertical thrust that supports the body, whilst the lateral component of the field causes only a compression of the body. Thus, if the ratio of the horizontal to the vertical component is low, the plate is suspended at a lower level and a greater power is transmitted to it. Further consideration shows that, in the case of a single-loop inductor, as the power applied to the inductor is increased and the metallic body rises, the power transmitted to it first decreases and then rises again. It is important that the metallic body suspended in the field should have lateral stability, which is not achieved in the simple cases so far considered. The inductors of practical interest are those in which the metal can hang stably in the field.

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The metallic body is displaced from a region of strong field to one of weak field or as it were, rolls down a 'hollow' in the field. Inductors for melting levitated metals may be classified into three types according to the relationship between the power transmitted to the body and the power applied to the inductor. One type consists of two co-planar rings connected in parallel with currents flowing in opposite directions. In a particular case the rings were of 120 and 210 mm internal diameter and the suspended metal was a disc of 150 mm diameter weighing 460 g. The outer coil was used to stabilise the disc. As the disc moves vertically the field at its surface remains constant, it is horizontal at the lower surface and zero at the upper because the disc thickness is much greater than the depth of penetration of the field. Thus the power applied to the body should remain constant and this is in fact found to be the case. The second type of inductors are those shaped like a boat or cradle consisting of two vertical coils connected in parallel and shaped like a cradle. The ends of the inductor are bent vertically upwards to make the suspended cylindrical body stable in the axial direction. With an inductor of this

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type an increase in the power applied to the inductor reduces the power absorbed by the body. Only after the body has risen a considerable distance above the lower conductors is there an appreciable increase in the power intake of the metal. The third type of inductor again has two vertical loops but one is crossconnected, so that whereas in the second type the upper pair of conductors both carry current in the same direction, in this type diametrically opposite conductors carry current in the same direction. In this type of inductor the metal body undergoes symmetrical compression by the electromagnetic field. As the power applied to the inductors is increased, the field intensity at the body surface increases on all sides and so the transmitted power increases. Comparison of test results for similar specimens at a frequency of 2 500 c/s shows that for a given power applied to an inductor of this cross-connected type, the maximum power transmitted to the body is at least four times greater than that of the 'cradle' type. Thus the cross-connected type should be used to produce high temperatures. The design of inductors for melting metals in the levitated condition has special features.

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In suspending a liquid body it is necessary that the hydrostatic pressure should be equalised by the electromagnetic at every point of the surface. The weight of suspended liquid metal is limited by its surface tension and specific gravity. To increase the efficiency of the system the size of the inductor should be quite small and to avoid the liquid metal sticking to the inductor conductors the field must be symmetrical. The current-carrying leads distort this symmetry and weaken the field in places. To restore the symmetry various devices are used, such as false leads placed opposite the real ones or displacement of the centres of the upper and lower rings of the inductor, and so on. It is desirable that the bottom of the inductors should be at equal potentials, otherwise the metal at the bottom of the inductor will initially short-circuit the portions at different potential, which can cause sparking and contamination of the hot metal by copper A special 'boat' type of construction is used to set up an equipotential bottom. As before, increasing the power applied to the inductor reduces the power transmitted to the molten metal and this somewhat limits its field of application

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The boat-type inductor is very convenient for series melting but the maximum temperature of the molten metal is lower than in a cross-connected inductor. In experiments with the 'boat' construction at a frequency of 70 kc/s, the metal could be raised to a temperature of 1500°C, and at a frequency of 200 kc/s to 2000°C. Therefore, as previously mentioned, the cross-connected inductor should be used to obtain higher temperatures. Two types have been developed, one with the coils connected in parallel and the other connected in series. In neither type is it possible to develop an equipotential bottom as in the boat conductor. However, the low voltage on the lower coil and the high contact resistance between the inductor conductors and the still cold solid metal practically prevents sticking of the metal to the inductor. At the instant of switching-on, the metal jumps and hangs in the field. In the inductor with parallel-connected coils the maximum potential difference between conductors is less than in that with series coils and, therefore, the parallel construction is more reliable in operation. However, the series connection can give higher temperatures. The limiting temperature for an inductor Card 9/12

Inductors for heating and melting

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with parallel cross-connected coils at a frequency of 200 kc/s was 2500°C and for the series version 3000°C. This difference arises partly from heavier losses in the leads to the parallel case and partly from the higher magnetic pressure above the suspended metal body in the series case. In the latter the current is the same in both turns whereas in the parallel connection the current in the upper turn is less than that in the lower because of the difference in diameter. The following table gives data on the melting of various metals in inductors of different designs and the weight of the samples.

Metal	Density g/cm ³	Melting point C	Weight [∰] g	Type of inductor
Titanium	4.5	1720	12	Boat
Zirconium	6.5	1850	12	it.
Chromium	7.1	189 0	15	II.
Vanadium	6. o	191 0	12	II .
Rhodium	12 4	1966	10	11:
Niobium	8.5	2420	10	Parallel cross-
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Series cross-connected 2630 10.2 Molybdenum 11 11 8 3000 16.6 Tantalum 11 11 ** 3400 19.8 Tungsten

Weight of liquid metal levitated
 Levitated in solid condition but did not melt.

There are 8 figures, 1 table and 6 references: 4 Soviet and 2 non-Soviet. The English-language references read as follows: Ref. 5: Okress E.C., Wroughton D.W., Comenetz G., Brace P.H., Kelly J.C.R. Electromagnetic Levitation of solid and molten metals. J. Appl. Phys. 1952, v.23, No.5, pp.545-552; Ref. 6: Harris B. Sc. and Jenkins A.E. Controlled atmosphere levitation system. J. Scient. Instrum. 1959, v.36, May, pp.238-240.

SUBMITTED: February 9, 1961

Card 11/12

TYULYAYEV, V.N., kand.tekhn.nauk; PAVLOV, N.A., inzh.

Operating reliability of tractor engines with the combustion chamber in the piston. Trakt. i sel'khozmash. no.914-5 S '65.

(MIRA 18:10)

1. Vsesoyuznyy nauchno-issledovatel skiy institut mekhanizatsii sel'skogo khozyaystva.

PAVLOV, N.A., inzh.; SLUKHOTSKIY, A.Ye., doktor tekhn. nauk

Calculation of the distribution of temperatures along the cross section of cylindrical steel objects during induction heating. Izv. vys. ucheb. zav.; energ. 8 no.6:17-22 Je '65. (MIRA 18:7)

1. Leningradskiy elektrotekhnicheskiy institut imeni Ul'yanova (Lenina), Predstavlena kafedroy slektrotermicheskikh ustanovok.

ARKHANGORGESKIY, L.A.; BUKSHTIYN, YA.A.; VOROBYYEV, S.V.; GAYENKO, F.A.; DOLGOV, Ye.N.; ZHIGLIN, A.A.; ZUBCVSKIY, G.F.; ISHKOV, I.G.; KRYZHANCVSKAYA, G.L.; LISTRATOV, A.A.; LURYYE, R.I.; MORGZOV, N.P.; CSTROZETSER, A.S.; PAVLOV, N.A.; PETROV, L.M.; POPCV, V.N.; TAKTAKOVSKIY. L.A.; TAUBE, D.N.; KHANIN, L.T.; SHAPIRO, TS.G.; SHVZYTSBURG, A.A.; SHEVTSOV, V.D.; DENISENKOVA, L.M., red.

[Assembler's handbook on performing mechanical assembly and special work on grain elevators and grain processing enterprises] Spravochnik montazhnika; po proizvodstvu mekhanomontazhnykh i spetsial'nykh rabot na elevatorakh i predpriatiiakh po pererabotke zerna. Moskva, TSentr. in-t nauchno-tekhn. informatsii i tekhniko-ekon. issl., 1963. 519 p. (MIRA 17:7)

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EMEMURIS, Dah. [Humphries, John].; ZAKHAROVA, Ye.G., [translator].; PAVLOV,

N.A., [translator].; AFAHAS'YEV, Yu. A., kand. tekhn. nauk, red.;

UEYEV, M.H., red., SOKOLOVA, T.S., tekhn. red.

[Rockets and guided missiles] [Translated from the English] Raketnye dvigateli i upravliaemye snariady. Moskva, Izd-vo inostr. lit-ry, 1958. 302 p.

(Missiles)

(Rockets(Aeronautics))
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"APPROVED FOR RELEASE: Tuesday, August 01, 2000

CIA-RDP86-00513R001239

ACC NRI AR6029492	SOURCE CODE: UR/0137/66/000/006/D011/D011
THOR: Pavlov, N. A.	4
TLE: Heat calculations for th	e induction heating of a rolled plate
OURCE: Ref. zh. Metallurgiya,	Abs. 6D81
	ta tokov tyoskoy chastoty, vyp. 6, 1965, 25-42
OPIC TAGS: induction heating,	hot rolling, me tal heat treating it
RANSLATION: A scheme was proporticel plates. The process of hitages, characterized by the districte: "cold", intermediate a ould also be used for low temporate or two initial stages. Expended on cylindrical samples should be a superfect of the color of the temperating the temperature drop did not	igh temperature induction heating was divided into three stribution of current across the section of the heated and "hot" cycles of induction heating. This method erature heating calculations, which may be composed of erimental confirmation of a similar heat calculation moved that during heating to surface temperatures of ture drop of 70-200°C, the relative error in determinate exceed 30-40%. This result as fully acceptable since curacy of 5-8% in the determination of the absolute value mperatures. An example of the calculation was present-
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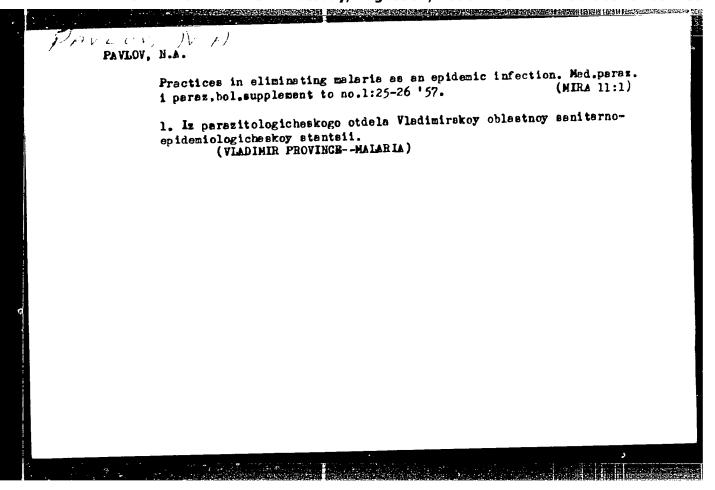
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AL'TSHULER, Z.Ye., inzh.; BASTUNSKIY, M.A., inzh.; BERSTEL', V.N., inzh.; BIRENBERG, I.E., inzh.; BOGOPOLSKIY, B.Kh., inzh.; BUKHARIH, S.I., inzh.; GERSHTEYN, B.G., inzh.; GRINSHPUH, L.V., inzh.; UREYYER, G.I., inzh.; DINERSHTEYN, A.G., inzh.; ZLATOPOL'SKIY, D.S., iznh.; KLANYUK, A.V., inzh.; KOZIN, Yu.V., inzh.; LEVITIN, I.P., inzh.; MEL'NIKOV, L.F., inzh.; MEL'KUMOV, L.G., inzh.; MADEL', M.B., inzh.; PAYLOV, N.A., inzh.; PASIEN, D.A., inzh.; PESIN, B.Ye., inzh.; PYATKOVŠKIY, P.T., inzh.; RAZNOSCHIKOV, D.V., inzh.; ROZENOYER, G.Ye., inzh.; ROZENBERG, R.L., inzh.; ROYTENBERG, N.L., inzh.; RYABINSKIY, Ye.I., inzh.; SYPCHENKO, I.I., inzh.; TARACHNIKOV, L.D., inzh.; FEL'DMAN, E.S., inzh.; SHTRAKHMAN, G.Ye., inzh.; SHTERENGAS, N.S., inzh.; LEVITIN, I.P., otvetstvennyy red.; STEL'MAKH, A.N., red.izd-ve; BEKKER, O.G., tekhn.red.

[Overall mechanization and automatization of production processes in the coal industry] Kompleksnaia mekhanizatsiia i avtomatizatsiia proizvodatvennykh protsessov v ugol'noi promyshlennosti. Pod red. IU.V.Komina i dr. Moskva, Ugletekhizdat, 1957. 82 p. (MIRA 11:3)

1. Gosudarstvennyy proyektno-konstruktorskiy institut. 2. Institut Giprouglesvtomatizatsiya i Tekhnicheskogo Upravleniya Ministerstva ugol'noy promyshlennosti (for all except: Levitin, Stel'makh, Bekker)

(Automatic control) (Coal mining machinery)



PAVLOV, A.H.

USSR/Processes and Equipment for Chemical Industries - K-2

Control and Measuring Devices. Automatic Regulation.

Abs Jour : Ref Zhur - Khimiya, No 2, 1957, 6989

Author : Pavlov, N.A.

Inst :

Title : Thermocouple with Open Hot Junction for High Pressures

Orig Pub : Sudostroyeniye, 1956, No 6, 36

Abstract : A distinctive feature of the thermocouple having an iner-

tia from fractions of a second to 2-3 seconds is the fact that the terminal ends of thermoelectrodes are hermetically sealed with sintered powdered enamel or enamel and glaze disposed in layers. Such thermocouples have been in operation for one year and a half at 225 atmospheres, absolute, and 375°, while under laboratory conditions they have been tested at pressures up to 500 atmospheres, absolute. They can be recommended for temperature determi-

nations up to 500-550°.

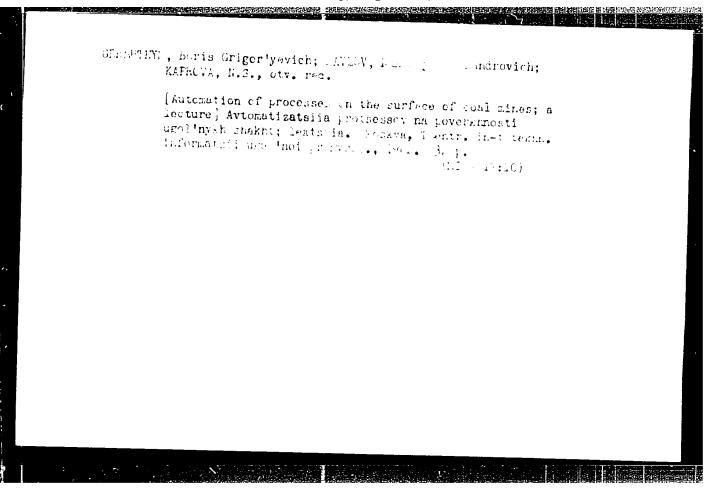
Card 1/1

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FOGEL', A.A. (Leningrad); FAVLOV, N.A (Leningrad); KORKIN, I.V. (Leningrad); SIDOROVA, T.A. (Leningrad)

Inductors for heating and melting metals in suspension. Izv.Ah SSSR.Otd.tekh.nauk.Mot.i topl. no.5:51-61 S-0 '61.

(MIRA 14:10)

(Magnetic induction) (Electrometallurgy)
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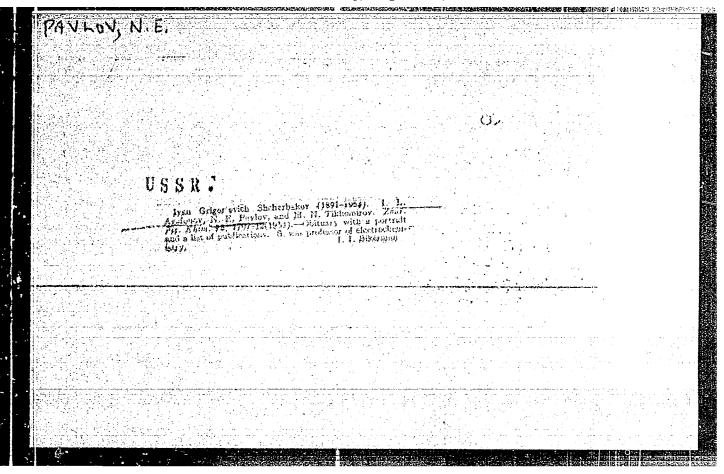


DYMARSKIY, L.Yu.; DIL'MAN, V.M.; ZALESSKAYA, L.T.; ZIV. M.A.; BOGIBOV, Ye.A.; PAVLOVA, M.V.

Combined hormone and chomotherapy and radiotherapy of far advanced breast cancer. Vop. onk. 9 no.7842-52 163.

(MIRA 16:11)

1. Iz Instituta onkologii AMN SSSR (nauchnyy rukowoditel' rabe'; chlen-korrespondent AMN SSSR prof. S.A. Kholdin). Adres autorows Leningrad, P-129, Institut onkologii AMN SSSR.



"APPROVED FOR RELEASE: Tuesday, August 01, 2000 CIA-RDP86-00513R001239

USSR/Scientists - Electrochemistry Card 1/1 Pub. 147 - 27/27 Authors Agafonov, I. L.; Pavlov, N. E.; and Tikhomirov, M. N. VERSETA WELLES Title 1 Ivan Grigoryevich Shcherbakov Periodical: Zhur. fiz. khim. 28/9, 1707-1712, Sep 1954 Abstract An sulogy honoring the death of I. G. Shcherbakov (1891-1953), famous Soviet electrochemist, is presented. List of major works by I. G. Shcherbakov is included, Institution: Submitted

"APPROVED FOR RELEASE: Tuesday, August 01, 2000 CIA-RDP86-00513R001239

Fenomen revosplameneniya i otekas pyaten posle nikotinovoy kisloty pri ranney diagnostike lepry. Vestnik venerologii i dermatologii, 1949, No. 5, s. 45-47

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PAVIOV, N.F., dots.; SHIMANOVICH, A.N.

Solusulphone (sulphetrone) in the treatment of leionyoma of the skin. Sov. med. 21 no.7:131-133 J1 '57. (MIRA 12:3)

1. Iz kafedry kozhnykh i venericheskikh bolezney (zav. - dots. H.F. Pavlov) Belorusskogo instituta usovershenstvovaniya vrachey (dir. - prof. M.H. Zhukova).

(SKIN, NEPZIASNS, ther.

leiomyoma, ther., sulphetrone (Rus.))

(SULFONES, ther. use

sulphetrone in skin leiomyoma (Rus.))

(INIONYO'4A, ther.

sulphetrone in skin leiomyoma (Rus.))
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SELISSKIY, Aleksandr Borisovich, prof.; PAVLOV, N.F., dots., red.; ZAYTSEVA, T., red. izd-va; VOLOKHANOVICH, I., tekhm. red.

[A guide to skin diseases; clinical aspects and treatment of diseases of the skin, pharmacotherapy and prescription filling] Spravochnik po kozhnym bolezniam; klinika i lechenie zabolevanii kozhi, farmakoterapiia i retseptura. Izd.2., perer. i dop. Minsk, Izd-vo Akad.nauk BSSR, 1961. 412 p.

(MIRA 15:1)

(SKIN-DISEASES)

PAVLOV, N.F., dotsent

Fungoid bromoderma, Vest. derm. 1 ven. 38 no.3:79-81 Mr *164.*

(N*RA 18:4)

1. Kafedra dermato-venerologii (zav. - dotsent N.F.Pavlov)

Belorusskogo instituta usovershenstvovaniya vrachey.

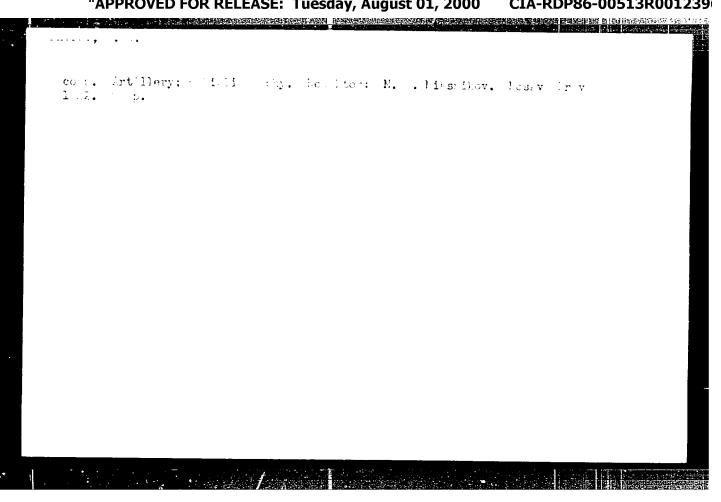
PAVLOV, N.G.

Limit diameters of blocks and drums of hoisting machines, Trudy LPI no.236:84-90 '64.

Selecting cores for hoisting cables. Ibid.:91-98

(MIRA 18:3)

"APPROVED FOR RELEASE: Tuesday, August 01, 2000 CIA-RDP86-00513R001239



A STATE OF THE PERSONS ASSESSED.

GEL'FENBEYN, Yakov Vladimirovich; VINITSKIY, D.Ya., inzh., retsenzent; EBERLIN, L.A., inzh., retsenzent; PAVLOV, N.G., red.; ZHITNIKOVA, O.S., tekhm. red.

[Hoisting mechanisms and rigging devices for the construction of thermal electric power plants]Gruzopod"emnye mekhanizmy i takelazhnye prisposobleniia dlia stroitel'stva teplovykh elektrostantsii. Moskva, Gosenergoizdat, 1962. 270 p.

(MIRA 15:9)

1. Moskovskiy filial Vsesoyuznogo instituta po proyektirovaniyu organizatsiy energeticheskogo stroitel'stva (for Vinitskiy, Eberlin).

(Hoisting machinery)
(Electric power plants-Design and construction)

ESCHER FOR THE PROPERTY OF THE

PAVLOV, N. G.

Cand Tech Sci - (diss) "Problem of the calculation and designing of plate separators with mechanized discharging of concentrated precipitates." Leningrad, 1961. 14 pp; (Ministry of Higher and Secondary Specialist Education RSFSR, Leningrad Technological Inst of the Refrigeration Industry); 180 copies; price not given; (KL, 5-61 sup, 192)

LANG, A.G.; MAZOVER, I.S.; MAYZEL', V.S.; BARANOV, N.A.; GOKHEER, M.M., dokt. tekhm. nauk, prof., retsenzent;; PAVLOV, N.G., kand. tekhm. nauk, red. MITARCHUK, G.A., red. izd-va; SICHETININA, L.V., tekhm. red.

[Cantry cranes; design and construction] Portal'nye krany; raschet i konstruirovanie. Izd.2., perer. i dop. Moskva, Mashgiz, 1962. 283 p. (MIRA 15:10)

(Cranes, derricks, etc.)

PAVLOV, Nikolay Germanovich [Armed forces of NATO]Vooruzhennye sily NATO. Leningrad, Ob-vo po rasprostraneniiu polit. i nauchn. znanii RSFER, 1959. Al p. (MIRA 15:9) (North Atlantic Treaty Organization)

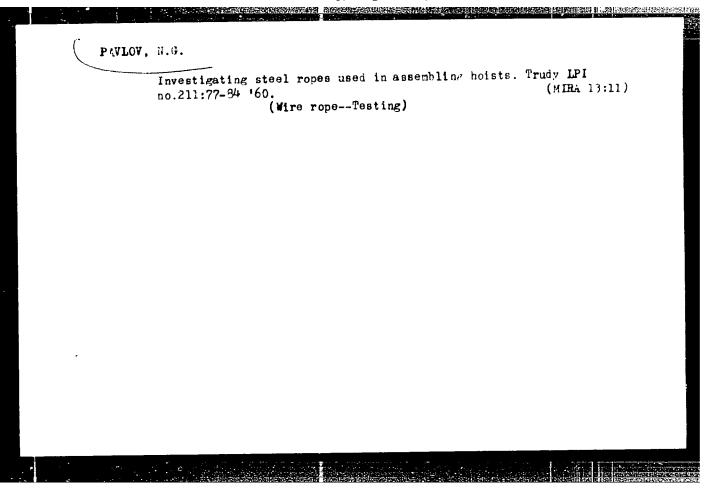
PAVLOV, N. G.

"A. S. Popov, the Great Russian Scientist and Inventor of Radio" (Velikiy russkiy uchenyy izobretatel' radio A. S. Popov), Central Polytechnic Library, 1949 6 pp.

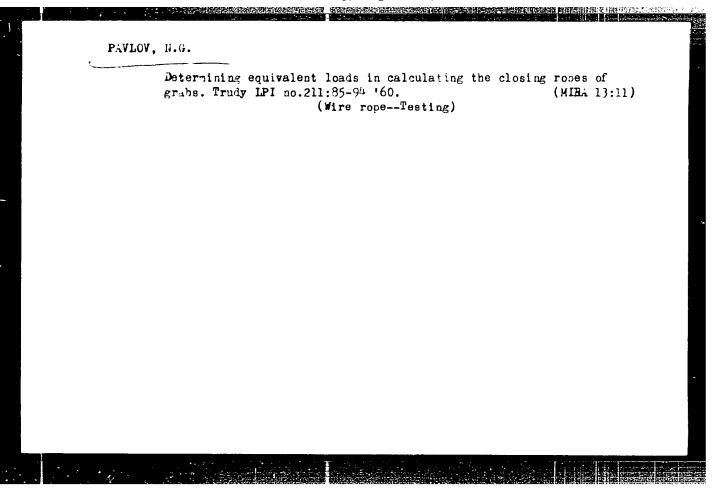
ROZULIN, E.A., doktor tekhn. nauk, prof.; PAVLOV, E.G., insh.

Determining the performance of ultra centrifuges from thickened deposits. Khim. mash. no.6:23-26 E-D '59. (MIRA 13:3) (Centrifuges) (Separators (Machines))

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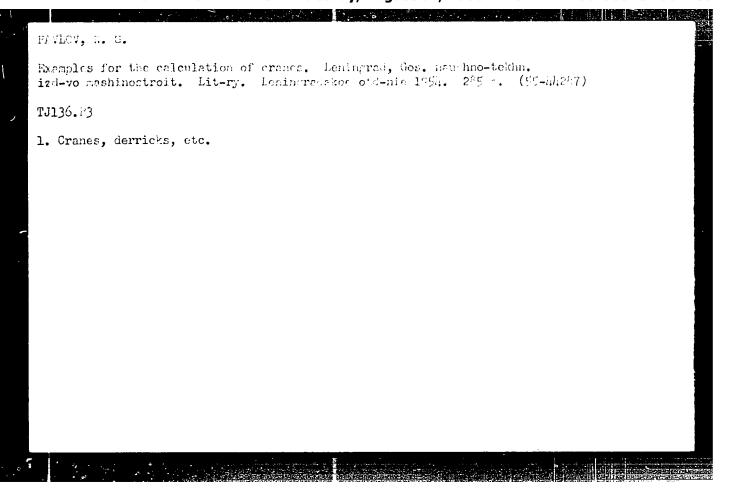
PAVIOV, Nikolay Georgiyevich, dotsent, kand, tekhm. neuk; MAYZEL', V.S., inzh., retsenzent; IANG, A.G., dots., red.; VASIL'YEVA, V.P., red. izd-va; SPERANSKAYA, O.V., tekhm. red.

[Examples of crans designs] Primery raschetov kranov. Izd.2., perer. i dop. Moskva, Gos. neuchno-tekhm. izd-vo mashinostroit. lit-ry, 1961. 301 p.

(Electric cranss)

(Electric cranss)

"APPROVED FOR RELEASE: Tuesday, August 01, 2000 CIA-RDP86-00513R001239



PAULOU, N.G

PAVLOV. N.G., kandidat tekhnicheskikh nauk, dotsent; LANG, A.G., inzhener, retsenzent; CHILAYEV, G.A., inzhener, redaktor; SOKOLOVA, L.V., tekhnicheskiy redaktor

[Examples of crane calculations] Primery raschetov kranov. Moskva.

Gos. nauchno-tekhn. izd-vo mashinostroitel noi lit-ry, 1954. 285 p.

(Cranes, derricks, etc.)

(MLRA 8:4)

SAMOYLOVICH, Platon Aleksendrovich; Pavlov, N.G., redaktor; MELETEV, A.S., redaktor izdatel'stva; Tikhonova, fe.Z., tekhnicheskiy redaktor

[Technical operation and maintenace of hoisting and conveying machinery] Tekhnicheskaia ekspluatatsiia i montazh pod*emno-transportnykh mashin. Izd. 2-oe, perer. i dop. Moskva, Izd-vo *Morskoi transport.* 1955. 345 p. (MIRA 9:8)

(Hoisting machinery (Conveying machinery)

20501 \$/050/61/000/005/001/003

3.5000 (1093,1041)

AUTHOR:

Pavlov, N.I.

TITLE:

The problem of cyclone and anticyclone movement

D235/D301

PERIODICAL: Meteorologiya i gidrologiya, no. 5, 1961, 24-26

TEXT: One of the important problems in synoptic practice is the determination of the direction and speed of cyclone and anticyclone movement. All research in this field mainly aims at establishing definite rules, by means of which the movement of "baric" or pressure formations may be forecast. Practice has shown that S.I. Troitskiy's "rule of leading flow" /Abstractor's note: No reference given is only applicable to some extent in baric formations developed at low levels, over whose centers the leading flow is clearly expressed: this rule is not applicable for high baric formations. Kh.P. Polosyan and N.L. Taborovskiy /Abstractor's note: No reference given sub-sequently found that the trajectory

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The problem of cyclone ...

of a deepening cyclone possesses cyclone curvature while the trajectory of a charging cyclone possesses anticyclone curvature. A.F. Lyubyuk Abstractor's note: No reference given has shown that deepening cyclones and weakening anticyclones are deflected to the left of the structure contour direction, passing through its center if the baric profile curvature at the earth's surface is greater than at the 700 mb surface. Charging cyclones and strengthening anticyclones, however, are deflected to the right under these conditions. If the isobar curvature at the earth's surface is less than the 700 atmosphere structure-contour, deepening cyclones and weakening anticyclones are deflected to the right and charging cyclones and strengthening anticyclones to the left. A more precise and objective forecast of the movement of baric centers may be obtained from the theoretical formulae for determining the components of the velocity of movement:

> dx di dy - dy didxdy (1)(1) $\left(\frac{\partial^{2} p}{\partial x \partial y}\right)^{2} - \frac{\partial^{2} p}{\partial x^{2}} \frac{\partial^{2} p}{\partial y^{2}}$

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20501

The problem of cyclone ...

\$/050/61/000/005/001/003 D235/D301

$$c_{y} = \frac{\frac{\partial^{2} p}{\partial y} \frac{\partial^{2} p}{\partial x^{2}} - \frac{\partial^{2} p}{\partial x} \frac{\partial^{2} p}{\partial x^{2} \partial y}}{\left(\frac{\partial^{2} p}{\partial x \partial y}\right)^{3} - \frac{\partial^{2} p}{\partial y} \frac{\partial^{2} p}{\partial x^{2} \partial y}}.$$
 (2)

The most complex part of the calculation of the velocity of movement of baric centers from these formulae lies in determining the

which characterize the variation of baric tendencies along the Xand Y-axes in relation to the cyclone center. As is known, the cyclone center as a specific point in the baric field is characterized by very low pressure values and is determined by equations

 $\frac{1}{\sqrt{y}} = 0; \quad \frac{1}{\sqrt{y}} = 0.$ It is known from synoptic practice that the passage of cyclone

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The problem of cyclone ...

\$/050/61/000/005/001/003 D235/D301

centers through any particular point is accompanied by calm weather. If the wind velocity is taken in a geostrophic approximation, it is clear from (3) that for the cyclone center both U_g and $V_g = 0$. Thus, for the cyclone center the equations of movement with no calculation of friction forces in a geostrophic approximation in the x, y, p and t coordinate system may be written as

 $\frac{\partial \mathbf{u}_{\mathbf{g}}}{\partial \mathbf{t}} + \tau \frac{\partial \mathbf{u}_{\mathbf{g}}}{\partial \mathbf{p}} = 0; \quad \frac{\partial \mathbf{v}_{\mathbf{g}}}{\partial \mathbf{t}} + \tau \frac{\partial \mathbf{v}_{\mathbf{g}}}{\partial \mathbf{p}} = 0.$ (4)

Here the value τ represents the vertical velocity at the cyclone center. Determining the values of

 $\frac{\partial^2 \mathbf{p}}{\partial \mathbf{x} \partial \mathbf{t}}, \quad \frac{\partial^2 \mathbf{p}}{\partial \mathbf{y} \partial \mathbf{t}}$

from (4) and inserting them in (2), we obtain formulae for determining the components of the velocity of movement of baric centers:

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20501 S/050/61/000/005/001/003 D235/D301

The problem of cyclone ... $c_{x} = \frac{v_{x} \left(\frac{\partial p}{\partial x \partial y} \frac{\partial^{2} H}{\partial p \partial y} - \frac{\partial^{2} p}{\partial y^{2} \partial p \partial x}\right)}{\left(\frac{\partial p}{\partial x \partial y}\right)^{2} - \frac{\partial^{2} p}{\partial y^{2} \partial x^{2}}}$

 $\epsilon_{y} = \frac{\epsilon_{p} g \left(\frac{\partial^{2} p}{\partial x \partial y} \frac{\partial^{2} H}{\partial p \partial x} - \frac{\partial^{2} p}{\partial x \partial y^{2}} \frac{\partial^{3} H}{\partial p \partial y} \right)}{\left(\frac{\partial^{2} p}{\partial x \partial y} \right)^{3} - \frac{\partial^{2} p}{\partial x \partial y^{2}} \frac{\partial^{3} H}{\partial y^{2}}}$ (5)

We present the values $\frac{\partial^2 H}{\partial p \partial x}$, $\frac{\partial^2 H}{\partial p \partial y}$ in finite forms, thereby taking into account that within the cyclone center at the earth's surface both

 $\frac{\partial H}{\partial X} = 0, \text{ and } \frac{\partial H}{\partial V} = 0:$ $\frac{\partial H}{\partial P \partial X} = -\frac{\frac{\partial H_p}{\partial X}}{\frac{\partial H_p}{\partial P \partial Y}}, \frac{\partial H}{\partial P \partial Y} = 0:$ $= -\frac{\partial H_p}{\partial Y}$ (6)

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The problem of cyclone ...

Inserting (6) in (5), we obtain the final formulae:

$$c_{x} = \frac{\operatorname{sp} R \left(\frac{\partial H_{p}}{\partial x} \frac{\partial p}{\partial y^{2}} - \frac{\partial H_{p}}{\partial y} \frac{\partial^{3} p}{\partial x \partial y} \right)}{\left(p_{0} - p \right) \left[\left(\frac{\partial^{2} p}{\partial x \partial y} \right)^{3} - \frac{\partial^{3} p}{\partial x^{2}} \frac{\partial^{2} p}{\partial y^{2}} \right]}$$

$$c_{y} = \frac{\operatorname{sp} R \left(\frac{\partial H_{p}}{\partial y} \frac{\partial p}{\partial x^{2}} - \frac{\partial H_{p}}{\partial x} \frac{\partial^{2} p}{\partial x \partial y} \right)}{\left(p_{0} - p \right) \left[\left(\frac{\partial^{2} p}{\partial x \partial y} \right)^{3} - \frac{\partial^{2} p}{\partial x^{2}} \frac{\partial^{2} p}{\partial y^{2}} \right]}$$

$$(7)$$

For determining $\frac{\partial^H p}{\partial x}$, $\frac{\partial^H p}{\partial y}$, during daily forecasting, the level H_p should be taken not arbitrarily, but depending on the characteristic vertical velocities in this layer (when w=1 cm/sec, $\triangle t=8.64 \cdot 10^4$ and $H_p=864$ m). In view of the nearness of the Card 6/11

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The problem of cyclone ...

standard 850 mb isobaric surface, this may be used for determining $\frac{\partial H_p}{\partial x}$, $\frac{\partial H_p}{\partial y}$, thereby allowing some error. Having set the X-axis tangentially to the 850 mb structure-contour over the cyclone center and the Y-axis at right angles to this tangent, the formulae for baric formations with circular isobars may be written in the form

$$c_{x} = -\frac{\tau_{p} g \frac{\partial H_{p}}{\partial x}}{(p_{0} - p) \frac{\partial^{2} p}{\partial x^{2}}} = 0;$$

$$c_{y} = -\frac{\tau_{p} g \frac{\partial H_{p}}{\partial y}}{(p_{0} - p) \frac{\partial^{2} p}{\partial y^{2}}}.$$
(8)

The value of represents the evolution of the baric formations. Upward vertical movements are observed in deepening cyclones and Card 7/11

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The problem of cyclone ...

in cyclones whose depth is not changing and downward vertical movements in charging cyclones. Since the calculation of the values of τ is very laborious, formulae (7) and (8) may be used principally for determining the direction of movement of baric formations. In order to determine the velocity of movement of baric formations, it is necessary to use the empirically established relationship between the wind velocity in the middle layers of the troposphere and the velocity of movement of baric formations at the earth's surface. The following conclusions may be drawn from an examination of formula (8): 1) When $\tau = 0$ the velocity of movement of the baric centers equals zero; 2) When $\tau < 0$ (deepening of a cyclone, strengthening of an anticyclone or stable pressure at the center) the baric formations move in a direction normal to the 850 atmosphere structure-contour counterclockwise; 3) When $\tau > 0$ (charging of a cyclone, weakening of an anticyclone) the baric formations move clockwise in a direction normal to the 850 atmosphere structure-contour; 4) When $\frac{1}{12}$

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The problem of cyclone ...

i.e. if the cyclone axis is quasi-vertical, the velocity of movement of the baric formations equals zero; 5) The greater the

value of $\frac{\partial H_D}{\partial y}$ (the stronger the wind at the 850 mb level over the center of the baric formations), the greater the velocity of movement; 6) The greater the value of τ (upward and downward vertical movements), the greater the displacement velocity; 7) The more rarefied the isobars in relation to the surface center of the cyclone, the greater the velocity of movement. It should be noted that these formulae are correct for a small time interval, since the angle of inclination of the vertical axis of the baric formations varies with time, as does the cyclone depth and the associated thickening and thinning of the isobars relative to the cyclone center both at the earth's surface and at higher levels. The author considers the example of a 24-hour forecast of the movement of a cyclone. According to observational data on the weather map at 3 o'clock on October 26, 1958, a cyclone center

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The problem of cyclone ...

with a pressure of about 981 mb was situated near Tobol'sk. The cyclone axis was inclined to the S.W., the leading flow at the 700 mb level over the cyclone center being oriented to the N.W. The wind velocity over the surface center of the cyclone at the 700 mb level was 30 km/hr. Clearly expressed isallobaric foci were observed in the for-ward and rear parts of the cyclone, the line joining their centers being oriented to the N.E. The 850 atmosphere structure contour over the surface center of the cyclone on the map was also oriented in a N.W. direction. It might have been assumed from an analysis of the altitude and surface maps that the cyclone would become approximately 5 mb deeper during the next 24 hours. On the basis of formulae (8) the cyclone should have moved to the N.E. at right angles to the direction of the 850 atmosphere structure-contour, with a speed of 30 km/hr, and at 3 o'clock on November 27 /Abstractor's note: This could be a printer's error, the center should have been in the region to the west of the Agan River (right tributary of the Ob').

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The problem of cyclone ...

According to the rule of leading flow, the cyclone should have moved N.W. in 24 hours to the area of the upper reaches of the Pechora River. Actually the cyclone had moved N.N.E. after 24 hours to the Lake Pyasu To area; during these 24 hours the cyclone moved at a mean velocity of 32 km/hr. According to formulae (8) the error in the direction of movement of the cyclone center was about 320, the locational error being about 450 km. According to the rule of leading flow the error in the direction of cyclone movement was about $60^{\rm o}$, and the locational error for the cyclone center was about $800~{\rm km}$. Abstractor's note: This is essentially a complete translation.

Card 11/11

ACCESSION NR: AR4008217

s/0169/63/000/011/B024/B024

SOURCE: RZh. Geofizika, Abs! 11B151

AUTHOR: Pavlov, N. I.

TITLE: Conditions for the regeneration of cyclones in the Kara Sea region during the period it is open to navigation

· }

CITED SOURCE: Sb. Probl. Arktiki i Antarktiki. Vy*p. 13. L., Morsk. transport,

TOPIC TAGS: meteorology, Arctic navigation, Kara Sea navigation, cyclonic regeneration, Arctic cyclonic regeneration, cyclone recurrence, seasonal cyclone

TRANSLATION: The author examines cases of cyclone regeneration occurring in 1950-1959. A table of the distribution of regenerative cyclones by months is constructed. The maximum occurs in September (16 cases). No regeneration was observed in July. Regeneration is most frequent and intensive in the southern part of the Kara Sea in the Ob'-Yenisey region, and in the central portion of the Sea. Cyclone regeneration in the region of the Kara Sea often occurs as a

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ACCESSION NR: AR4008217

result of the sucking in of the Arctic front into the system of the regenerative cyclone, as well as when the young cyclone enters the region of an old cyclone. Four indications of regeneration are given. An actual example is considered. I. Dubina.

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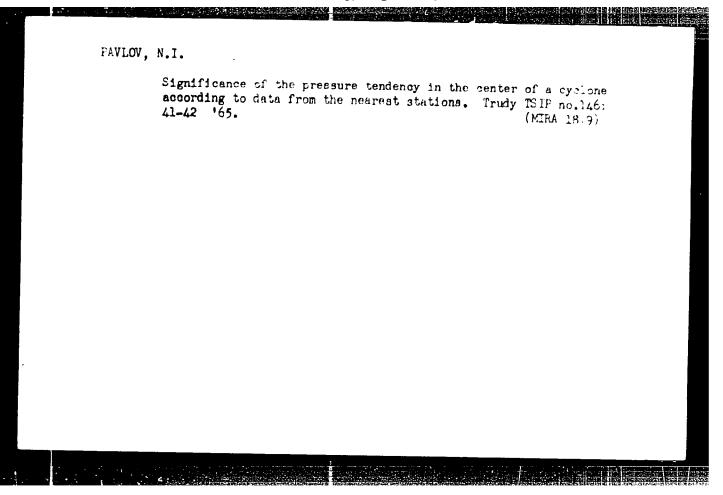
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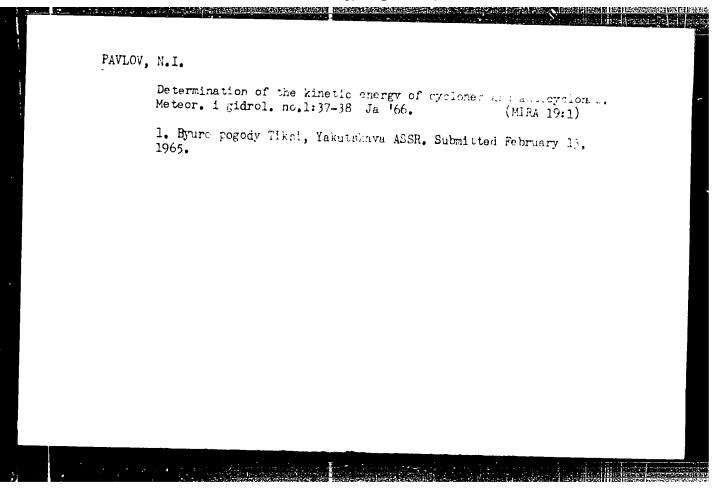
Cord 2/2

PAVLOV, N.I.

Contribution of vertical movements to the evolution of cyclones and anticyclones. Meteor, i gidrol. no.5:49-50 My 164. (MIRA 1775)

1. Byuro pogody, Tiksi.





IJP(c) GS EWI (m)/ENA (m)-2 \$/0000/64/000/000/0693/0697 ACCESSION NR: AT5007947 AUTHOR: Zinov'yev, L. P.; Issinskiv, I. B.; Kotov, V. I.; Kulakova, Ye. M. Pavlov, N. I.; Myznikov, K. P. TITLE: The utilization of parametric resonance in the 10-Bev synchrophasotron for particle output SOURCE: International Conference on High Energy Accelerators. Trudy. Hoscow, Atomizdat, 1964, 693-697 TOPIC TAGS: high energy accelerator, electron paramagnetic resonance, focusing accelerator ABSTRACT: Accelerated particles with pulse length of less than 100 psec are of great importance in current physical experiments. Great interest is shown in the possibility of applying the parametric (half-integral) resonance. Such a possibility has been discussed in the literature especially in application to conditions of weak-focusing and strong-focusing accelerators. Utilization of the resonance $v_x = \frac{1}{2}$ for the rapid hurling of the accelerated beam against the traget in a small 70-Mev synchrotron permitted one to obtain good results. The present report discusses the results of investigations conducted on the synchrophasotron at the Card 1/3

L 3776-66 ACCESSION NR: AT5007947

Joint Institute of Nuclear Research to clarify the expediency of artificially exciting the resonance $v_{\mu} = \frac{1}{2}$ for hurling the accelerated particles against the target and for extracting the proton beam from the accelerator's chamber. The resonance conditions were created by way of variation in an identical manner of the field index n in two neighboring quadrants such that the mean value of n in the accelerator corresponded to the condition of resonance. The resonance force here is determined by the magnitude of the first harmonic of the excitation (A. A. Kolomenskiy, A. N. Lebedev, Teoriya tsiklicheskikh uskoriteley (Theory of Cyclical Accelerators), Hoscow, Fizmatgiz, 1952). Under real conditions the exciting field was created with the help of windings arranged inside the accelerator's vacuum chamber. The inductance of the windings arranged to about 3 mega-henries, which limited the rate of growth of the excitation. Numerical calculations carried out on an electronic computer on the exact equations of motion of the particles in the magnetic field showed that, for obtaining the resonance conditions, it is necessary to create the configuration of the magnetic field such that the index n in the excited quadrants reach values close to 0.9 for a duration of 300 microseconds (about 400 revolutions). The following topics are discussed: the dependence of the field index # upon the radius for currents of 340 amperes and none in the ex-

L 3776-66 ACCESSION NR: AT5007947 citer winding; radial hurling of particles on the target 10 cm and 20 cm from the target; dependence of the duration of beam collision with the target upon the radial position of the target relative to the orbit for various excitations; dependence of the depth of hurling upon excitation and radial position of the target; the angle of flight of the particles into the gap of the deflector as a function of the moment of flight. "The authors thank Academician V. 1. Veksler for his helpful discussions; L. A. Smirnova and N. N. Govorum for their help in the numerical computations; V. H. Buldakovskiy, A. I. Kryukov, Yu. F. Kusagin, V. S. Mironov, M. I. Hikitayev, et al., for their participation in developing and adjusting the emulsion experiments." Orig. art. has: B figures. ASSOCIATION: Ob" yedinennyy institut yadernykh issledovaniy, Dubna (Joint Institute of Muclear Research) SUBMITTED: 26May84 ENCL: OD SUB CODE: no ret sov: OTHER: 003 Card 3/3

	AUTHOR: Zinov'yev, L. P.; Issinskiy, I. B.; Kotov, V. I.; Kulakova, Ye. 15.; Myzailov, K. P.; Pavlov, N. I.
	TITLE: Fast extraction of the proton-supel-state 19
	SOURCE: Pribory i tekhnika eksperimenta, no. 1, 1965, 33-38
	TOPIC TAGS: particle beam, proton synchrotron, beam extraction
	ABSTRACT: Fast extraction of the beam and sending it to a target located near the maximum-deflection azimuth was achieved by creating parametric-resonance conditions in the weak-focusing 10-Gev proton-synchrotron. The resonance conditions were ensured by windings placed inside the vacuum chamber. A bank of capacitors was discharged at 10 kv into the winding; by the end of the acceleration cycle, the (thyratron-switched) winding current rose sine-wise to a maximum and then (also thyratron-switched) fell-off exponentially. The system ensured a
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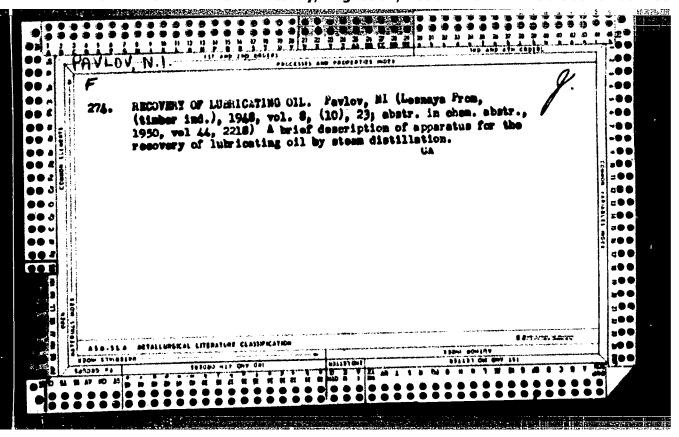
	ACCESSION NR: AP500702	20		9	• .
	beam-extraction time as for	was 30 msec. "The a	uthors wish to thank V.	, I ,	
-	great help in calculations:	and V. N. Buldakovski	and N. N. Governm for	their	•
	Land Street, V. D. MILLOHOV, M.	l. I. MITHERVOY, and of	hore who took mand to at		
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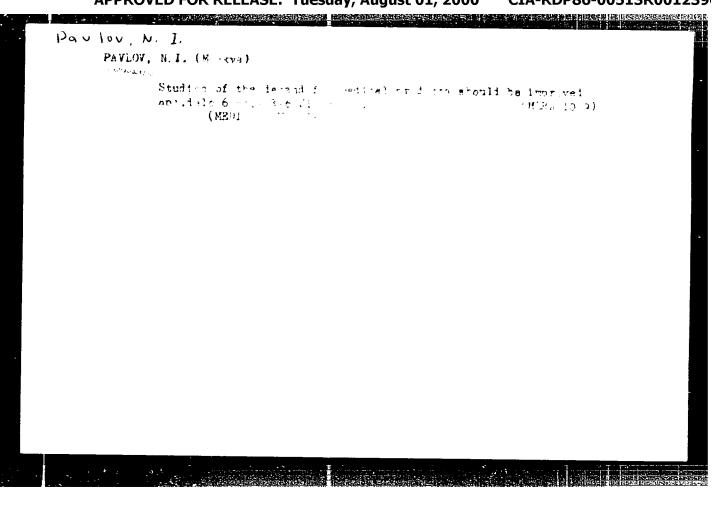
BABINOV, B.I.; PAVLOV, E.I., redaktor; VOLMHOVER, R.S., tekhnicheskiy redaktor

[Work experience of an efficient lathe operator] Opyt tokaria-skorostnika. Moskva, Goslesbunizdat, 1951. 30 p. [Microfilm] (Turning)

(Turning)

(MIRA 7:10)





24(6)

AUTHORS:

Rzhanov, A. V., Pavlov, N. W., Selezneva, M. A.

507/57-58-12-1/15

TITLE:

Investigation of the Energy Levels and of the Effective Capture Cross Sections of the Surface Recombination Levels in Germanium (Issledovaniye energeticheskikh polozheniy i effektivnykh secheniy zakhvata poverkhnostnykh

rekombinatsionnykh urovney v germanii)

PERIODICAL:

Zhurnal tekhnicheskoy fiziki, 1958, Nr 12, pp 2645-2656 (USSR)

ABSTRACT:

An investigation of the surface recombination levels occurring as a consequence of heating the germanium samples in vacuum or because of the action of ozone upon these samples was carried out. Preliminary data on the temperature dependence of the energy levels and of the effective capture cross sections when a hole and an electron are captured by these levels and the dependence of these characteristics on the cross-field amplitude were obtained. The supposition is expressed that the charges captured at the slow levels at the surface have a considerable influence upon the characteristics of the surface recombination levels. From this supposition is deduced that the nature of the recombination levels occurring because of

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Investigation of the Energy Levels and of the Effective Capture Cross Sections of the Surface Recombination Levels in Germanium

507/57-58-12-1/15

heating in vacuum is the same as the nature of the levels caused by the action of ozone. A considerable parallelism between concentration and charge of "slow" surface levels and the concentration of the recombination levels was found. There are 9 figures, 2 tables, and 10 references, 3 of which

ASSOCIATION:

Fizicheskiy institut imeni P. N. Lebedeva AN SSSR Moskva (Physics Institute imeni P. N. Lebedev, AS USSR, Moscow)

SUBMITTED:

December 28, 1957

Card 2/2

THE REPORT OF THE PROPERTY OF

- 1. POVLOV, N. M.
- 2. USSR (600)
- 4. Electric Substantions
- 7. Shortcomings of 3-6-10 My standard transfer requests as for all directs procedures. From . or all 9 no. 12, 1952.

Lista and discusses 6 uneconomical features and other tesign left formed in plans for series of standard 3-7-10-kv transformer substations levelore; or Giproshakhtoproyekt of Finistry of Gal Industry. This land catherage is great for the deficiencies listed.

9. Monthly List of Aussian Accessions, Library of Longres, earth 1953. Unclassified.

PAVLOV, E.M.; VIADIMIROVA, Ye. F.

Reflect of sleep therapy of function of the visual organ, Vest. oft., Moskva 31 no. 5:13-17 Sept-Oct 1952. (CIML 23:3)

1. Professor for Pavlov; Departmental Physician for Vladimirova, 2. of the Rye Clinic of Stavropol' Medical Institute.

PAVIOV, N.H.; HOICHANOVA, L.A.

Damages of the visual organs in children in rheuratism. Vest. oft., Moskva 32 no.4:14-21 July-Aug 1953. (CIML 25:1)

1. Professor for Pavlov; Departmental Physician for Molchanova. 2. Of the Clinic for Eye Diseases of Stavropol' Medical Institute.

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PAVLOV, N.M., professor

Studies on reactivity of the organism in glaucoma, Vest. oft.
33 no.3:5-14 My.Je '54. (MIRA 7:6)

1. Lirektor glaznoy kliniki Stavropol'skogo meditsinskogo instituta.

(GLAUCOMA, physiology,

*reactivity of organism in)
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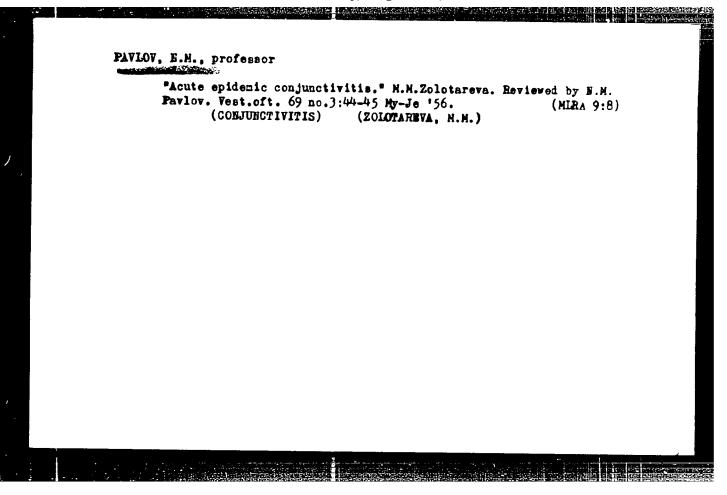
PAVLOV, N.N., professor.

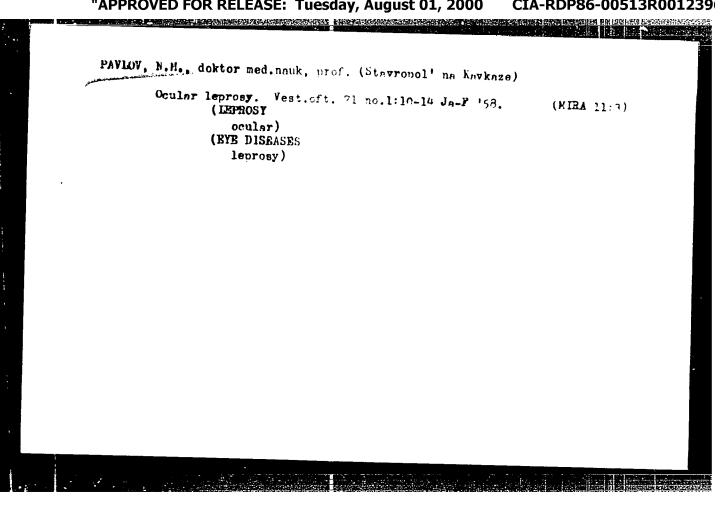
Medical tactics in ophtalmology. Trudy AN Tadah. SSR 40:65-70 '55.

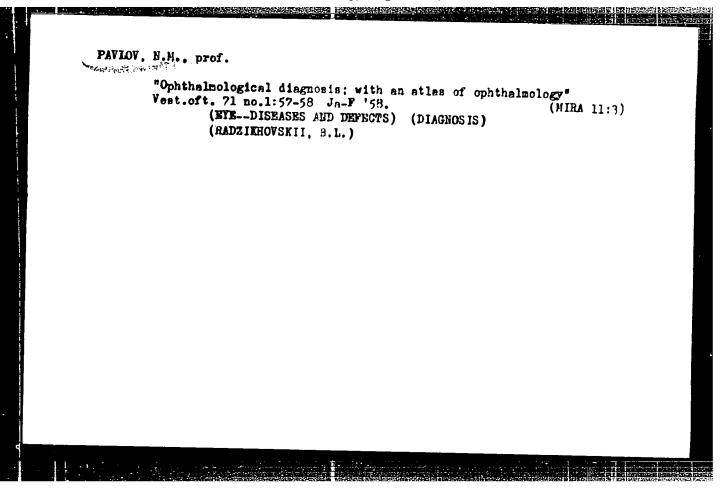
(MIRA 9:10)

1. Zavednyshchiy kafedroy glasnykh bolesney Stavropol'skogo meditsina skogo instituta (dir.- prof. V.A. Chepurin).

(OPHTAIMOLOGY) (MEDICINE--PRACTICE)





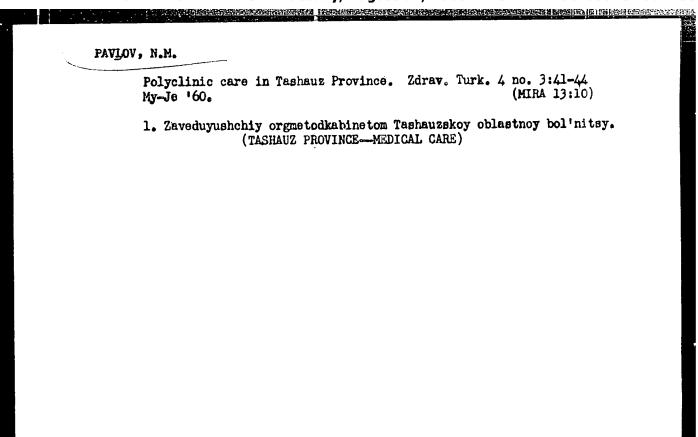


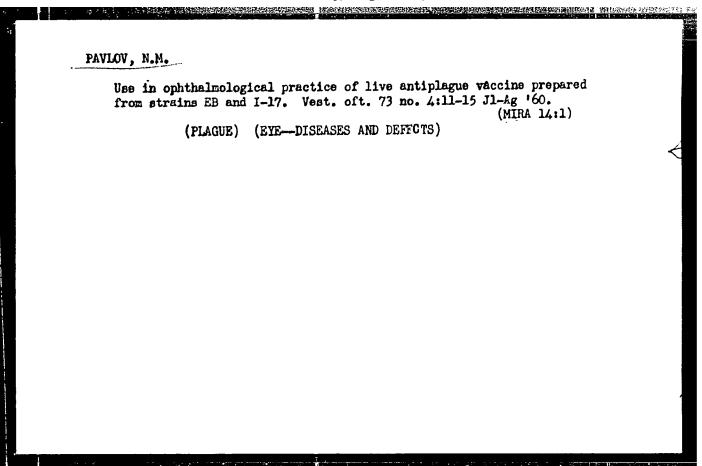
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PAVLOV, E.M., prof. (Stavropol')

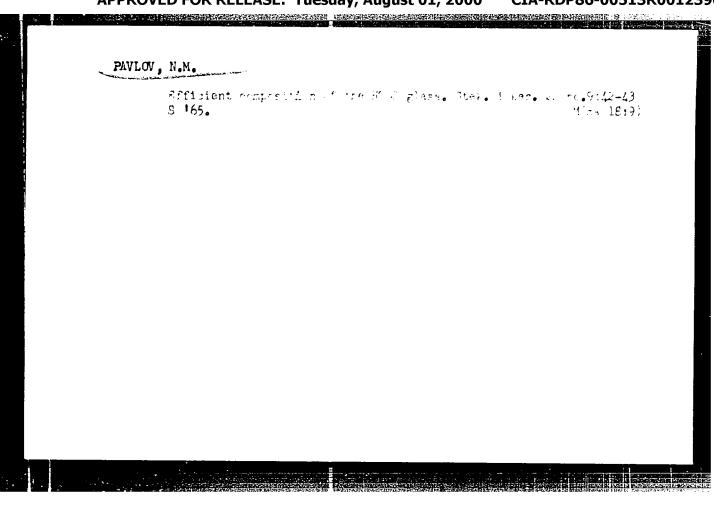
Bulgarian ophthalmology and ophthalmologists. Vest.oft. 72 no.1:
59-61 Ja-F '59.

(OPHTEALMONOLOGY,

in Bulgaria (Rus))
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(A) EWT(1)/EWT(m)/EWP(t)/EWP(b) IJP(c) ACC NR JD/WW/GG AP6000182 SOURCE CODE: UR/0032/65/031/012/1450/1451 AUTHOR: Iglitsyn, H. I.; Ivanova, I. I.; Konstantinova, G. Ye.; Kosaganova, H. G.; ORG: State Scientific Research and Design Institute of Rare Metals Industry (Gosudarstvennyy nauchno-issledovatel'skiy i proektnyy institut redkometatallicheskoy promyshlennosti) TITLE: Determination of nitrogen content in a-SiC by EPR technique SOURCE: Zavodskaya laboratoriya, v. 31, no. 12, 1965, 1450-1451 TOPIC TAGS: silicon carbide, EPR, Hall effect, nitrogen, single crystal ABSTRACT: An attempt was made to use EPR technique for determining nitrogen content in single crystals of hexagonal silicon carbide (a-SiC). The method is based on determining the number of paramagnetic centers (nitrogen atoms) in a crystal sample by comparing its EPR spectrum with the spectrum of a reference sample (CuSO, ·SH2O). Both spectra were taken at the liquid nitrogen temperature with a PE 1301 radiospectrometer The relationship between the concentration of the free charge carriers at room temperature as determined from the Hall effect (nHall) and the concentration of non-compensated and non-ionized nitrogen centers at the liquid mitrogen temperature (MEPR) is:

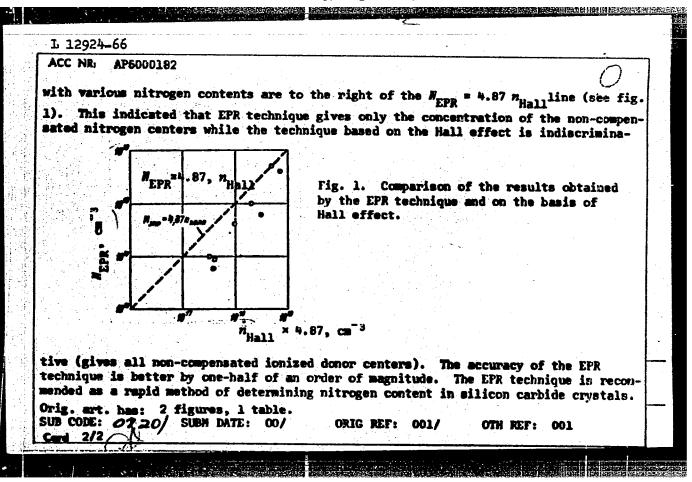
= 4.87 n Hall. All the experimental results obtained with silicon carbide samples

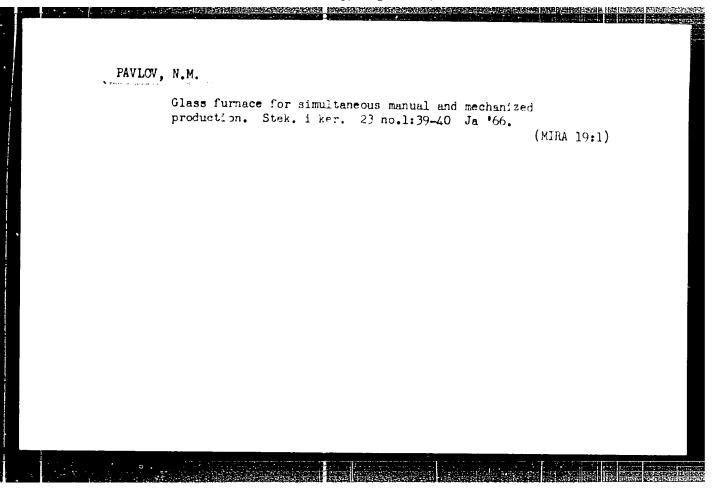
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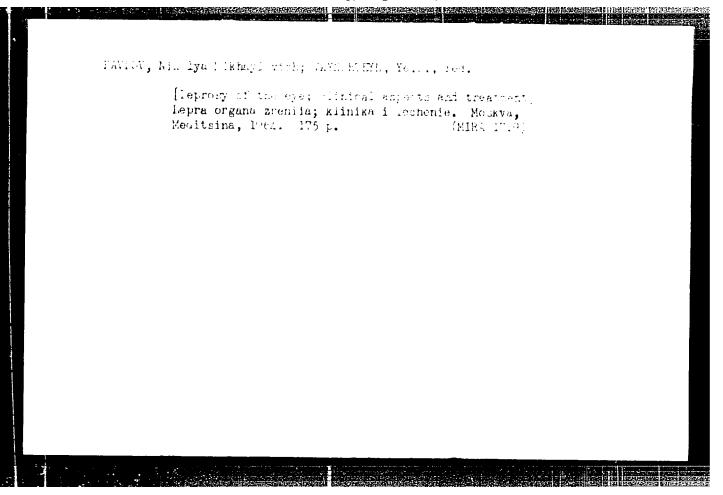
APPROVED FOR RELEASE: Tuesday, August 01, 2000

Cord 1/2

CIA-RDP86-00513R0012396







PAVLOV, H. H., Aspirant

"Analysis of and Heasures to Promote Electrical Safety During the Use of Excavators Under Conditions Frevailing in Coal Pits." Cand Tech Sci. Noscow Order of Lenin Power Engineering Inst imeni V. H. Melotov, 3 Dec 97. (V., 23 Nov 54)

Survey of Scientific and Technical Pissertation Defended by USSR Ligher Educational Institutions (11)

SC: Sum. No. 521, 2 Jun 55

PAVIOV, N.N., kand, tekhn. nauk.

Arc-suppression coils used in high-voltage networks in the Czechoslovak Republic. Vest, elektroprom. 27 no.8:75-76 Ag '56.

(MLRA 10:9)

1. Moskovskiy energeticheskiy institut im. Molotova.

(Czechoslovakia--Electric coils)

PHOLENAN,

110-9-12/23

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AUTHOR:

Kopylov, I.P., Candidate of Technical Sciences, Paviov, N.N., Candidate of Technical Sciences

A Method of Regulating the Inductance of Grounding Coils. TITLE:

(Sposob regulirovaniya induktivnosti zazemlyayushchikh katu-

shek)

Vestnik Elektropromyshlennosti, 1957, Vol.28, No.9, PERIODICAL: pp. 46 - 47 (USSR).

Grounding (or compensating) coils are becoming more widely ABSTRACT: used and recently they have been applied to mobile electrified machines supplied through cables such as excavators or electric tractors. The principles and advantages of compensating the capacitative component of fault current are briefly explained. The inductive reactance of the coil should equal the capacitative reactance of the lines, but as the capacitance of the system is continually varying, the coil should be adjustable for complete compensation under all operating conditions. The simplest solution is to instal on each part of the circuit a compensating coil, tuned to resonance and switched with the line. However, even in this case the individual coils will have to be adjustable. Adjustment may be by altering: the number of turns; the air gap; the relative position of the coils; the inductance of the coil by auxiliary magnetisation. Tapped coils can only be Card 1/3 adjusted in steps and tap-changing switches are bulky and